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RESEARCH ARTICLE

## Assessment of resource-saving technologies in low-tonnage chemical industries for compliance with best available technologies principles

Natalia A. Kostikova<sup>✉</sup>, Elena N. Glukhan, Pavel V. Kazakov, Maria M. Antonova, Dmitry I. Klimov

GosNIIOKhT, State Scientific Center of the Russian Federation, Moscow, 111024 Russia

<sup>✉</sup>Corresponding author, e-mail: [kutkin@gosniiookht.ru](mailto:kutkin@gosniiookht.ru)

### Abstract

**Objectives.** To develop a methodology for the quantitative assessment of new technologies in accordance with the principles of best available technologies (BAT). To evaluate the developed technologies of low-tonnage chemical production of tetramethylthiuram disulfide, N-cyclohexyl-2-benzothiazolylsulfenamide, diisopropyl xanthohene disulfide, and N-phenyl-2-naphthylamine for compliance with BAT principles and compare with alternative (implemented, known) technologies in terms of environmental impact.

**Methods.** A methodology for the quantitative assessment of new technologies for the production of organic substances in accordance with BAT principles was used.

**Results.** The developed methodology for the quantitative assessment of new technologies in accordance with BAT principles based on the calculation of comprehensive comparison indicators with alternative technologies for technological and environmental indicators allowed us to determine the level of implemented technologies for the production of tetramethylthiuram disulfide, N-cyclohexyl-2-benzothiazolylsulfenamide, diisopropyl xanthohene disulfide, and N-phenyl-2-naphthylamine to minimize the impact on the environment, including through the development of special technological solutions for resource conservation and waste reduction, and to conduct a quantitative assessment of the achieved environmental outcome. It is established that the

considered new technologies of low-tonnage chemical production comply with BAT principles and are more environmentally advanced compared to alternative ones previously implemented in the USSR.

**Conclusions.** For the first time, a methodology for quantifying new technologies in accordance with BAT principles is proposed. The possibility of its use at the stage of making basic technological decisions on the implemented production method in order to ensure compliance with legislative requirements for technologies in the field of environmental safety to achieve environmental protection goals is shown on the example of low-tonnage technologies for the production of tetramethylthiuram disulfide, N-cyclohexyl-2-benzothiazolylsulfenamide, diisopropyl xanthogen disulfide, and N-phenyl-2-naphthylamine created in GosNIIOKhT.

**Keywords:** low-tonnage chemical production technologies, quantitative assessment methodology, best available technologies (BAT) principles, tetramethylthiuram disulfide, N-cyclohexyl-2-benzothiazolylsulfenamide, diisopropyl xanthogen disulfide, N-phenyl-2-naphthylamine

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## НАУЧНАЯ СТАТЬЯ

# Оценка ресурсосберегающих технологий малотоннажных химических производств на соответствие принципам наилучших доступных технологий

Н.А. Костикова<sup>✉</sup>, Е.Н. Глухан, П.В. Казаков, М.М. Антонова, Д.И. Климов

Государственный научно-исследовательский институт органической химии и технологии, Москва, 111024 Россия

<sup>✉</sup> Автор для переписки, e-mail: [kutkin@gosniiokht.ru](mailto:kutkin@gosniiokht.ru)

## Аннотация

**Цели.** Разработать методику количественной оценки новых технологий в соответствии с принципами наилучших доступных технологий (НДТ). Провести оценку разработанных технологий малотоннажных химических производств тетраметилтиурамдисульфида, N-циклогексил-2-бензотиазолилсульфенамида, диизопропилксантогендисульфида и N-фенил-2-нафтиламина на соответствие принципам НДТ и сравнить с альтернативными (реализованными, известными) технологиями по уровню воздействия на окружающую среду (ОС).

**Методы.** Методика количественной оценки новых технологий производства органических веществ в соответствии с принципами НДТ.

**Результаты.** Разработанная методика количественной оценки новых технологий в соответствии с принципами НДТ на основании расчета комплексных индексов сравнения с альтернативными технологиями по технологическим и экологическим показателям позволила определить уровень внедряемых технологий получения тетраметилтиурамдисульфида, N-циклогексил-2-бензотиазолилсульфенамида, диизопропилксантогендисульфида и N-фенил-2-нафтиламина по минимизации воздействия на ОС, в том числе

за счет разработки специальных технологических решений по ресурсосбережению и снижению отходности, и провести количественную оценку достигаемого экологического результата. Установлено, что рассмотренные новые технологии малотоннажных химических производств соответствуют принципам НДТ и являются более экологически совершенными по сравнению с альтернативными, ранее реализованными в СССР. **Выводы.** Впервые предложена методика количественной оценки новых технологий в соответствии с принципами НДТ и показана возможность ее использования на этапе принятия основных технологических решений по внедряемому способу производства для обеспечения выполнения законодательных требований к технологиям в сфере экологической безопасности по достижению целей охраны ОС на примере созданных во ФГУП «ГосНИИОХТ» малотоннажных технологий производства тетраметилтиурамдисульфида, N-циклогексил-2-бензотиазолилсульфенамида, диизопропилксантогендисульфида и N-фенил-2-нафтиламина.

**Ключевые слова:** технологии малотоннажных химических производств, методика количественной оценки, принципы наилучших доступных технологий, НДТ, тетраметилтиурамдисульфид, N-циклогексил-2-бензотиазолилсульфенамид, диизопропилксантогендисульфид, N-фенил-2-нафтиламин

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## INTRODUCTION

One of the tasks of state industrial policy in the field of production consists in the introduction of resource-saving and environmentally friendly technologies according to the provisions of the Federal Law of December 31, 2014 No. 488-FL “On Industrial Policy in the Russian Federation”. The implementation of this policy is carried out by abandoning the use of outdated and inefficient technologies according to best available technologies (BAT) principles. BAT criteria are legally defined for evaluating technologies in terms of their environmental impact. Currently, the selection of BAT is carried out on the basis of expert assessments<sup>1</sup>. However, in order to substantiate BAT [1], present the BAT

selection process [2], and identify technologies as BAT-compliant [3], various models are proposed based on a systematic approach and the use of mathematical tools, as well as on conducting environmental and economic BAT analysis. In the context of the state reform of the environmental regulation system and in accordance with the concept of introducing BAT as the primary mechanism for implementing state policy in the field of environmental safety at the stage of new technology development, special attention should be paid to addressing issues involved in determining the level of harmful effects on the environment and the minimization of such harmful effects to standard BAT values. This becomes all the more relevant due to the legal assignment of the production of basic organic

<sup>1</sup> Decree of the Government of the Russian Federation of December 23, 2014, No. 1458 “On the procedure for determining technology as the best available technology, as well as the development, updating and publication of information and technical reference books on the best available technologies” (as amended by Decrees of the Government of the Russian Federation of September 9, 2015, No. 954; dated December 28, 2016, No. 1508; dated March 09, 2019, No. 250). URL: <http://www.consultant.ru/>. Accessed February 13, 2022 (in Russ.).

chemicals to areas of BAT application<sup>2</sup> and objects of category I (significant) in terms of their negative impact on the environment<sup>3</sup>.

These factors determine the relevance of conducting a preliminary assessment of new technologies to determine their compliance with modern environmental requirements. However, there is currently no methodological basis for such an assessment. The development and implementation of highly efficient resource-saving technologies for obtaining materials that are in demand by the industrial complex of the Russian Federation under conditions of low-tonnage industrial production is one of the main directions of scientific and practical activities of *GosNIIOKhT*. Ensuring the current level of implemented technologies to minimize the impact on the environment is achieved, among other things, by developing special technological solutions for resource saving and waste reduction. To assess the achieved environmental outcome, we have developed the “Methodology for the quantitative assessment of new technologies for the production of organic substances in accordance with BAT principles” [4].

Compliance with the approach for evaluating new technologies is determined on the basis of BAT principles by calculating comprehensive indicators of comparison with alternative (already implemented or known) technologies in terms of technological (amount of waste, emissions, and discharges) and environmental indicators (degree of use of raw materials and waste and the effectiveness of measures for the treatment of gas emissions and discharges into water bodies).

The evaluation of new technologies for compliance with environmental protection goals is a necessary but insufficient development element, since one of the key targets is achieving a high

level of efficiency. The “Methodology for the quantitative assessment of new technologies for the production of organic substances in accordance with economic and environmental efficiency criteria” developed in our previous work [5] can be used to determine the most effective option for organizing production based on the calculation of comparative economic and environmental efficiency coefficients. The comparative economic efficiency coefficient includes an assessment of the cost of raw materials and instrumentation of a technological process. The comparative environmental efficiency ratio reflects the achieved level of minimization of the negative impact on the environment during the implementation of the technology, as well as the cost effectiveness of ensuring this environmental outcome. At the same time, the assessment of the economic efficiency of environmental costs makes it possible to exclude unreasonably costly options in comparison with the obtained environmental outcome and ensure that the developed technological solutions comply with the BAT criteria.

This article discusses new technologies for the production of tetramethylthiuram disulfide, *N*-cyclohexyl-2-benzothiazolylsulfenamide, diisopropyl xanthogen disulfide, and *N*-phenyl-2-naphthylamine developed at *GosNIIOKhT*; technologies, as well as possible directions for their modernization.

## METHODS

The calculation of the main and additional indicators [4] for comparing the developed technologies (Table 1) was carried out using data from technological production regulations.

The final assessment of the developed technology was carried out by comparing the relevant indicators with those of the alternative (implemented or known) technology, while the consumption coefficients for raw materials and auxiliary materials, production waste generation rates, as well as basic and additional technological indicators, were determined on the basis of the material balances of these technologies.

Further, comprehensive indicators of comparison of the developed and alternative production technologies were calculated along with the final indicator of the assessment of the developed technology for compliance with BAT principles (Table 2).

Indicator  $K_1$  characterizes the degree of reduction of waste of the new technology in comparison with the existing alternative. Here, since the target

<sup>2</sup> Decree of the Government of the Russian Federation dated December 24, 2014 (as amended on May 24, 2018) No. 2674-r. “On Approval of the List of Areas of Application of the Best Available Technologies.” URL: <http://www.consultant.ru/>. Accessed February 17, 2020 (in Russ.).

<sup>3</sup> Decree of the Government of the Russian Federation “On approval of the criteria for classifying objects that have a negative impact on the environment as objects of categories I, II, III and IV” dated September 28, 2015, No. 1029. URL: <http://www.consultant.ru/>. Accessed February 17, 2020 (in Russ.).

<sup>4</sup> Decree of the Government of the Russian Federation of December 23, 2014, No. 1458 “On approval of the rules for determining technology as the best available technology, as well as the development, updating and publication of information and technical reference books on the best available technologies.” URL: <http://www.consultant.ru/>. Accessed September 09, 2022 (in Russ.).

**Table 1.** Main and additional technological indicators for comparing production technologies

| Indicator   | Indicator characteristics and calculation method  |
|---|---|
| Main technological indicators of production       |   |
| $A_T$   | Generation rate of solid and liquid waste, t/t, according to the regulations  |
| $B_T$   | Specific emissions into the atmosphere, t/t, according to the regulations   |
| $C_T$   | Wastewater generation rate, t/t, according to the regulations   |
| Additional technological indicators of production |   |
| $J_K$   | <p>The degree of complexity and completeness of the extraction of useful components from a feedstock is calculated as the sum of the recovery factors of the feedstock components, taking into account the yield and excluding technological losses of the product, t/t</p> $J_K = \sum_{i=1}^K J_i = \sum_{i=1}^K \frac{\sum_{\text{Rec}=1}^N P_i^{\text{Rec}}}{\sum_{\text{Raw}=1}^M P_i^{\text{Raw}}}$ <p>where <math>K</math> is the quantity of valuable components in the raw material; <math>N</math> is the number of product flows; <math>M</math> is the number of raw material flows; <math>P_i^{\text{Rec}}</math> is the amount of <math>i</math> useful substance, passed into finished products, t; <math>P_i^{\text{Raw}}</math> is the amount of <math>i</math> useful substance contained in raw materials, t</p> |
| $J_O$   | <p>The degree of utilization of generated waste is calculated as the share of the regenerated component in the total mass of waste, t/t, and calculated according to the material balance of the regeneration operation per single operation.</p> $J_O = \frac{\sum Q^{\text{Pr}} + \sum Q^{\text{P}}}{\sum Q^{\text{O}}},$ <p>where <math>\sum Q^{\text{Pr}}</math> is the amount of waste used in the production of other products, t/year, <math>\sum Q^{\text{P}}</math> is the amount of waste sold, t/year; <math>\sum Q^{\text{O}}</math> is the amount of generated waste, t/year.</p>  |
| $J_A$   | <p>The degree of purification of emissions of harmful substances into the atmosphere, which is calculated as the share of captured gases and vapors in the total mass of production off-gases, t/t, can be calculated from material balance data per operation.</p> $J_A = \frac{\sum V_i}{\sum V_j},$ <p>where <math>\sum V_i</math> is the total mass of captured emission components, t/year; <math>\sum W_k</math> is the total mass of substances contained in gas emissions formed during the production process, t/year</p>  |
| $J_B$   | <p>The degree of purification of discharges into water bodies is calculated by dividing the mass of discharges cleaned from harmful impurities to the total mass of their formation, t/t, using the material balance data per operation.</p> $J_B = \frac{\sum W_l}{\sum W_k},$ <p>where <math>\sum W_l</math> is the total mass of discharges, t/year; <math>\sum W_k</math> is the total mass of wastewater generated, t/year</p>   |



is to minimize waste, the values related to the developed technology are given in the numerator to ensure the ratio  $K_1 < 1$ .

The  $K_2$  indicator characterizes the increased complexity and completeness of the extraction of useful components using the new technology as compared to the existing alternative. Since the aim is to increase the level of raw material utilization, the values related to the developed technology are given in the denominator to ensure the ratio  $K_2 < 1$ .

The value of the final indicator for assessing the new (developed) technology  $I < 2$  supports the conclusion that the developed technology conforms with BAT principles and is more environmentally friendly than the existing alternative [4].

## RESULTS

Assessment of the compliance of the tetramethylthiuram disulfide production technology with the BAT principles

The technology for the production of tetramethylthiuram disulfide is based on the one-stage method for its preparation published in our previous work [6], which includes the condensation of

dimethylamine with carbon disulfide followed by peroxidation of the formed dimethyldithiocarbamic acid without its isolation.

The formation reaction of tetramethylthiuram disulfide is described by Scheme (1).

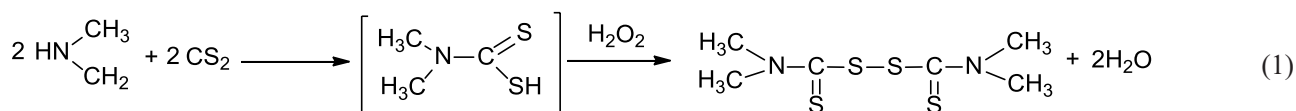
Condensation of dimethylamine with carbon disulfide is carried out at an equimolar ratio of components; peroxidation of the resulting dimethyldithiocarbamic acid is carried out at a molar ratio of dimethylamine : carbon disulfide : hydrogen peroxide equal to 1 : 1 : 0.55–0.57. The process is carried out in a methanol medium.

The calculation of the main and additional technological indicators of the production of tetramethylthiuram disulfide was carried out using the data of the “Temporary technological regulations for the pilot low-tonnage production of tetramethylthiuram disulfide based on domestic raw materials, No. TTR-3-350” on consumption coefficients for raw materials (Table 3) and waste generation rates (Table 4). The calculation data of the main and additional technological indicators of the production of tetramethylthiuram disulfide are presented in Table 5.

We carried out a final assessment of the developed technology for the production of tetramethylthiuram

**Table 2.** Comprehensive comparison indicators and the final indicator of the assessment of the developed technology for compliance with BAT principles

| Indicator  | Formula for calculating the indicator   |
|--|---|
| Comprehensive indicator of comparison of the main technological indicators of the developed and alternative technologies $K_1$   | $K_1 = \frac{1}{3} \left( \frac{A_{T,P}}{A_{T,A}} + \frac{B_{T,P}}{B_{T,A}} + \frac{C_{T,P}}{C_{T,A}} \right),$ <p>where <math>A_{T,P}</math>, <math>B_{T,P}</math>, <math>C_{T,P}</math> and <math>A_{T,A}</math>, <math>B_{T,A}</math>, <math>C_{T,A}</math> are specific indicators of waste, atmospheric emissions and discharges into natural waters for the developed and alternative technologies, respectively</p>                    |
| Comprehensive indicator of comparison of additional technological indicators of the developed and alternative technologies $K_2$ | $K_2 = \frac{1}{4} \left( \frac{J_{K,A}}{J_{K,P}} + \frac{J_{O,A}}{J_{O,P}} + \frac{J_{A,A}}{J_{A,P}} + \frac{J_{B,A}}{J_{B,P}} \right),$ <p>where <math>J_{K,P}</math>, <math>J_{O,P}</math>, <math>J_{A,P}</math>, <math>J_{B,P}</math> and <math>J_{K,A}</math>, <math>J_{O,A}</math>, <math>J_{A,A}</math>, <math>J_{B,A}</math> are additional technological indicators for the developed and alternative technologies, respectively</p> |
| Final indicator for evaluating the developed technology $I$  | $I = K_1 + K_2$   |



disulfide by comparing it with an existing method for obtaining the product by oxidation with hydrogen peroxide in the presence of sulfuric acid of the sodium salt of dimethyldithiocarbamic acid, which is synthesized by the reaction of dimethylamine with carbon disulfide in the presence of alkali at a molar ratio of carbon disulfide : dimethylamine : sodium hydroxide, equal to 1 : 1 : 1.03 [7]. The precipitate of tetramethylthiuram disulfide was filtered

off, washed, granulated, and dried [8]. This process was already implemented in the USSR at the Khimprom Volgograd production association [9].

Based on the calculated material balances, the consumption coefficients for raw materials and auxiliary materials (Table 6) were determined along with the waste generation rates for the production of tetramethylthiuram disulfide using an alternative technology (Table 7).

**Table 3.** Consumption coefficients for raw materials and auxiliary materials in the tetramethylthiuram disulfide production

| Name of raw materials   | Expense coefficients |       | Note                 |
|-------------------------|----------------------|-------|----------------------|
|                         | kg/operation         | t/t   |                      |
| Dimethylamine (33%)     | 72.2                 | 1.29  | –                    |
| Carbon disulfide        | 40.2                 | 0.73  | –                    |
| Hydrogen peroxide (37%) | 27.8                 | 0.50  | –                    |
| Methanol                | 4.5                  | 0.08  | With regeneration    |
|                         | 565.4                | 10.10 | Without regeneration |

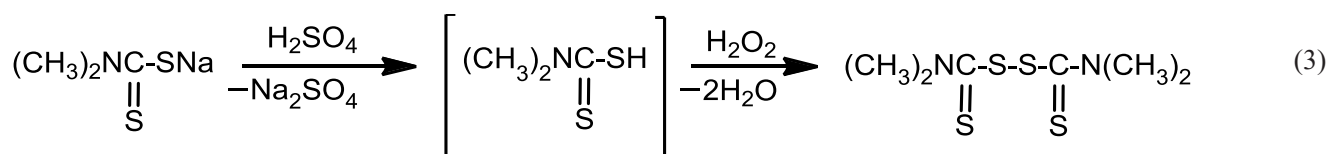
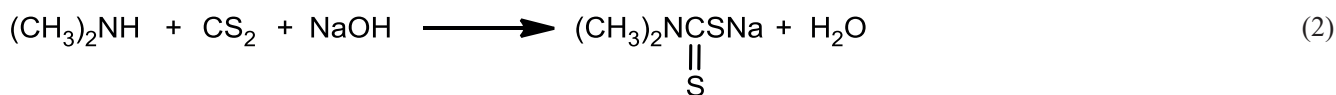
**Table 4.** Waste generation standards, emissions, and discharges in the tetramethylthiuram disulfide production

| Type of waste                        | Aggregate state of waste | Composition                  | Amount, % | Production waste generation rate |      |
|--------------------------------------|--------------------------|------------------------------|-----------|----------------------------------|------|
|                                      |                          |                              |           | kg/operation                     | t/t  |
| VAT residue of methanol regeneration | Liquid                   | VAT residue, including       | 100.00    | 83.9                             | 1.50 |
|                                      |                          | Water                        | 91.18     | 76.5                             | 1.37 |
|                                      |                          | Organic impurity             | 4.17      | 3.5                              | 0.06 |
|                                      |                          | Tetramethylthiuram disulfide | 4.65      | 3.9                              | 0.07 |
| Air emissions                        |                          | None                         |           |                                  |      |
| Wastewater discharge                 |                          | None                         |           |                                  |      |

**Table 5.** Basic and additional technological indicators calculated for the developed and existing alternative technologies used in the tetramethylthiuram disulfide production

| Indicator   | Calculation method and indicator value  |  |
|---|---|--|
|   | Developed technology  | Alternative technology                 |
| Main technological indicators of production   |   |  |
| Generation rate of solid and liquid waste   | $A_{T,P} = 1.5 \text{ t/t}$ (Table 4)   | $A_{T,A} = 4.58 \text{ t/t}$ (Table 7) |
| Specific emissions into the atmosphere  | Off-gases are locally cleaned in contact devices. Since the cleaning efficiency is 100%, there are no emissions into the atmosphere (Tables 4 and 7)  |  |
|   | $B_{T,P} = 0 \text{ t/t}$   | $B_{T,A} = 0 \text{ t/t}$              |
| Wastewater generation rate  | There is no wastewater discharge (Tables 4 and 7)   |  |
|   | $C_{T,P} = 0 \text{ t/t}$   | $C_{T,A} = 0 \text{ t/t}$              |
| Additional technological indicators   |   |  |
| Degree of complexity and completeness of the extraction of useful components from the feedstock | It is calculated as the sum of the extraction coefficients of dimethylamine $P_{DMA}$ and carbon disulfide $P_{CS_2}$ taking into account the yield of tetramethylthiuram disulfide (56.1 kg per operation, 95%) without taking into account technological losses of the product in the filtrate and washing solution.<br>$P_{DMA} = 0.41/0.43 = 0.95 \text{ t/t}$<br>$P_{CS_2} = 0.69/0.73 = 0.95 \text{ t/t}$<br>$J_{K,P} = 0.95 + 0.95 = 1.90 \text{ t/t}$<br>$J_{K,P} = 1.90 \text{ t/t}$ | $J_{K,A} = 1.90 \text{ t/t}$           |
| Degree of generated waste utilization   | It is calculated as the share of regenerated methanol in the total mass of waste according to the material balance of the methanol regeneration stage per one operation<br>$J_{O,P} = 558.2/644.9 = 0.87 \text{ t/t}$   | $J_{O,A} = 0.69 \text{ t/t}$           |
| Degree of purification of emissions of harmful substances into the atmosphere                   | It is calculated as the share of captured methanol vapors in the trap and in the process of local purification in contact devices in the total mass of off-gases, taking into account 100% efficiency of their purification (Tables 4 and 7)  |  |
|   | $J_{A,P} = 1.00 \text{ t/t}$  | $J_{A,A} = 1.00 \text{ t/t}$           |
| Degree of purification of discharges into water bodies  | There is no wastewater discharge (Tables 4 and 7)   |  |
|   | $J_{B,P} = 0 \text{ t/t}$   | $J_{B,A} = 0 \text{ t/t}$              |





**Table 6.** Consumption coefficients for raw materials and auxiliary materials in the tetramethylthiuram disulfide production using an alternative technology

| Name of raw materials   | Expense coefficients |      | Note                 |
|-------------------------|----------------------|------|----------------------|
|                         | kg/operation         | t/t  |                      |
| Dimethylamine (33%)     | 72.20                | 1.29 | —                    |
| Carbon disulfide        | 40.20                | 0.73 | —                    |
| Hydrogen peroxide (37%) | 27.80                | 0.50 | —                    |
| Sodium hydroxide (44%)  | 50.92                | 0.91 | —                    |
| Sulfuric acid (60%)     | 45.75                | 0.82 | —                    |
| Methanol (99.47%)       | 1.81                 | 0.03 | With regeneration    |
|                         | 240.00               | 4.28 | Without regeneration |
| Water                   | 76.97                | 1.37 | With regeneration    |
|                         | 412.00               | 7.34 | Without regeneration |

**Table 7.** Waste generation standards, emissions, and discharges in the alternative tetramethylthiuram disulfide production technology (with methanol and water regeneration)

| Type of waste                                 | Aggregate state of waste | Composition             | Amount, % | Production waste generation rate |      |
|---|--------------------------|-------------------------|-----------|----------------------------------|------|
|   |                          |                         |           | kg/operation                     | t/t  |
| VAT residue (methanol regeneration operation) | Liquid                   | VAT residue, including: | 100.00    | 7.57                             | 0.13 |
|   |                          | Water                   | 91.17     | 2.71                             | 0.05 |
|   |                          | Organic impurities      | 8.83      | 4.86                             | 0.09 |

Table 7. Continued

| Type of waste                              | Aggregate state of waste | Composition             | Amount, % | Production waste generation rate |      |
|--|--------------------------|-------------------------|-----------|----------------------------------|------|
|  |                          |                         |           | kg/operation                     | t/t  |
| VAT residue (water regeneration operation) | Liquid                   | VAT residue, including: | 100.00    | 249.46                           | 4.45 |
|  |                          | Sodium sulfate          | 15.95     | 39.78                            | 0.71 |
|  |                          | Water                   | 83.06     | 207.19                           | 3.69 |
|  |                          | Organic impurities      | 1.00      | 2.49                             | 0.04 |
| Air emissions                              |                          | None                    |           |                                  |      |
| Wastewater discharge                       |                          | None                    |           |                                  |      |

Further, we calculated comprehensive indicators for comparing the developed and alternative technologies used in the production of tetramethylthiuram disulfide along with the final indicator for evaluating the developed technology for compliance with BAT principles (Table 8).

The value of the final indicator  $I$  of the assessment of the new technology  $1.04 < 2$  supports the conclusion that the technology developed by us for the production of tetramethylthiuram disulfide meets BAT principles and is more environmentally friendly compared to the alternative one originally implemented in

the USSR [4]. The technology developed by us was introduced in the branch of *GosNIIOKhT—Separate Plant No. 4* (Novocheboksarsk, Chuvash Republic), whose experimental low-tonnage tetramethylthiuram disulfide production capacity is 5000 kg/year.

The high efficiency ( $K_1 = 0.11$ ) of the developed technology for the production of tetramethyl thiuram disulfide (Table 8) was determined by the low waste rate of the technological process. The achieved level of environmental friendliness of production ( $K_2 = 0.93$ ) was ensured by the regeneration of raw materials (methanol).

**Table 8.** Comprehensive indicators and the final evaluation indicator of the developed tetramethylthiuram disulfide production technology

| Indicator  | Calculation method and indicator value  |
|--|---|
| Comprehensive indicator of comparison of the main technological indicators of the developed and alternative technology $K_1$   | <p>Due to the absence of emissions of harmful substances into the atmosphere or discharges into water bodies for the developed and alternative technologies, no comparison of specific indicators of such emissions and discharges is carried out.</p> $K_1 = (A_{T,P}/A_{T,A})/3$ $K_1 = (1.50/4.58)/3 = 0.11$   |
| Comprehensive indicator of comparison of additional technological indicators of the developed and alternative technology $K_2$ | <p>Due to the absence of discharges of harmful substances into water bodies for the developed and alternative technologies, no calculation or comparison of the degree of purification of discharges into water bodies is carried out.</p> $K_2 = (J_{K,A}/J_{K,P} + J_{O,A}/J_{O,P} + J_{A,A}/J_{A,P})/3$ $K_2 = (1.9/1.9 + 0.69/0.87 + 1.00/1.00)/3$ $K_2 = 0.93$ |
| Technology assessment outcome $I$  | $I = 0.11 + 0.93 = 1.04$  |

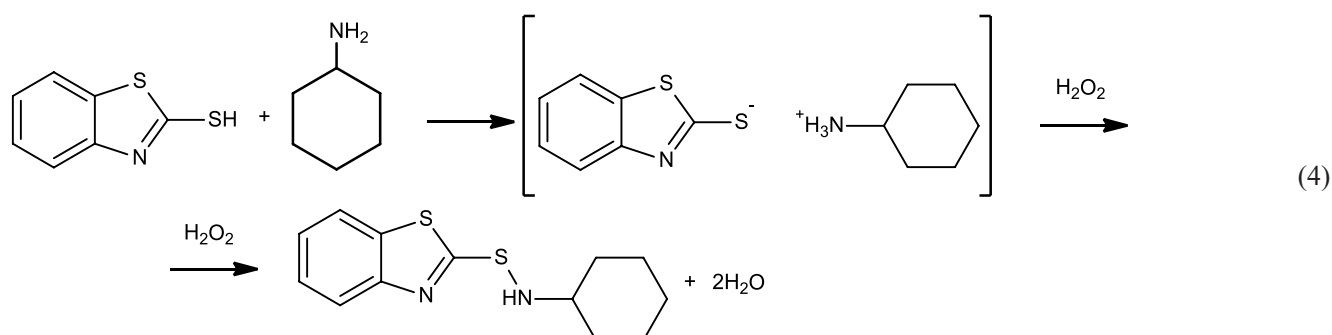
### Assessment of the compliance of the *N*-cyclohexyl-2-benzothiazolysulfenamide production technology with the BAT principles

The technology for the production of *N*-cyclohexyl-2-benzothiazolysulfenamide is based on the one-stage method for its preparation published in [9], which includes the condensation of 2-mercaptobenzothiazole and cyclohexylamine, followed by peroxidation of the resulting intermediate compound, cyclohexylammonium 1,3-benzothiazole-2-thiolate, without its selection. The process is carried out in an aqueous medium at a molar ratio of 2-mercaptobenzothiazole : cyclohexylamine : hydrogen peroxide equal to 1 : 3 : 1.1 and is described by Scheme (4).

The calculation of the main and additional technological indicators of the production of *N*-cyclohexyl-2-benzothiazolysulfenamide was carried out using the data of "Temporary technological regulations for pilot low-tonnage production of *N*-cyclohexyl-2-benzothiazolysulfenamide, No. TTR-5-350" on consumption coefficients for raw

materials (Table 9) and the generation rate of production waste (Table 10). The results of the calculation of the main and additional technological indicators are presented in Table 11.

The final assessment of the developed technology for the production of *N*-cyclohexyl-2-benzothiazolysulfenamide was carried out by comparing this technology with an alternative one based on the method of its production by the interaction of the sodium salt of 2-mercaptobenzothiazole (captax) with cyclohexylamine in the presence of sodium hypochlorite. The sodium salt of Captax was mixed with cyclohexylamine, the reaction mass was acidified with 37% hydrochloric acid. This gave the cyclohexylamine salt of Captax, which was oxidized with sodium hypochlorite in the presence of alkali. Unreacted cyclohexylamine was isolated from wastewater by nitrogen purge at a temperature of 120–130°C. The described method for the preparation of *N*-cyclohexyl-2-benzothiazolysulfenamide was implemented in the USSR at *Novokemerovo Chemical Plant* [11].



**Table 9.** Consumption coefficients for raw materials and auxiliary materials in the *N*-cyclohexyl-2-benzothiazolysulfenamide production

| Name of raw materials         | Expense coefficients |        | Note                 |
|-------------------------------|----------------------|--------|----------------------|
|                               | kg/operation         | t/t    |                      |
| 2-Mercaptobenzothiazole (97%) | 68.80                | 0.872  | –                    |
| Cyclohexylamine (99%)         | 33.31                | 0.422  | With regeneration    |
|                               | 119.99               | 1.521  | Without regeneration |
| Hydrogen peroxide (37%)       | 39.60                | 0.502  | –                    |
| Water                         | 0.00                 | 0.000  | With regeneration    |
|                               | 800.00               | 10.139 | Without regeneration |

**Table 10.** Waste generation standards, emissions, and discharges in the *N*-cyclohexyl-2-benzothiazolylsulfenamide production (with regeneration of water and cyclohexylamine)

| Type of waste                              | Aggregate state of waste | Composition             | Amount, % | Production waste generation rate |       |
|--|--------------------------|-------------------------|-----------|----------------------------------|-------|
|  |                          |                         |           | kg/operation                     | t/t   |
| VAT residue (water regeneration operation) | Liquid                   | VAT residue, including: | 100.00    | 64.76                            | 0.821 |
|  |                          | Water                   | 62.25     | 40.31                            | 0.511 |
|  |                          | Organic impurities      | 37.75     | 24.45                            | 0.310 |
| Air emissions                              |                          | None                    |           |                                  |       |
| Wastewater discharge                       |                          | None                    |           |                                  |       |

**Table 11.** Basic and additional technological indicators calculated for the developed and existing alternative technologies used in the *N*-cyclohexyl-2-benzothiazolylsulfenamide production

| Indicator   | Calculation method and indicator value  |  |
|---|---|--|
|   | Developed technology  | Alternative technology                     |
| Main technological indicators   |   |  |
| Generation rate of solid and liquid waste   | $A_{T,P} = 0.821 \text{ t/t}$<br>(Table 10)   | $A_{T,A} = 4.45 \text{ t/t}$<br>(Table 13) |
| Specific emissions into the atmosphere  | Abgases are absent, emissions into the atmosphere are absent (Tables 10 and 13)   |  |
|   | $B_{T,P} = 0$   | $B_{T,A} = 0$                              |
| Wastewater generation rate  | There is no wastewater discharge (Tables 10 and 13)   |  |
|   | $C_{T,P} = 0$   | $C_{T,P} = 0$                              |
| Additional technological indicators   |   |  |
| Degree of complexity and completeness of the extraction of useful components from the feedstock | It is calculated as the sum of the recovery factors of 2-mercaptobenzothiazole $P_{MBT}$ and cyclohexylamine $P_{CHA}$ taking into account the yield of <i>N</i> -cyclohexyl-2-benzothiazolylsulfenamide (78.9 kg per operation, 75%) and the regeneration of cyclohexylamine<br>$P_{MBT} = 0.632/0.846 = 0.75 \text{ t/t}$<br>$P_{CHA} = 1.447/1.506 = 0.96 \text{ t/t}$<br>$J_{K,P} = 0.75 + 0.96 = 1.71 \text{ t/t}$ | $J_{K,A} = 1.64 \text{ t/t}$               |

Table 11. Continued

| Indicator   | Calculation method and indicator value  |                        |
|---|---|------------------------|
|   | Developed technology  | Alternative technology |
| Degree of utilization of generated waste                                      | It is calculated as the share of regenerated cyclohexylamine and water in the total mass of waste (mother liquor) per one operation:<br>$J_{O,P} = (84.64 + 800)/949.40 = 0.93$ t/t | $J_{O,A} = 0.55$ t/t   |
| Degree of purification of emissions of harmful substances into the atmosphere | Abgases are absent, emissions into the atmosphere are absent (Tables 10 and 13)   |                        |
|   | $J_{A,P} = 0$ t/t   | $J_{A,A} = 0$ t/t      |
| Degree of purification of discharges into water bodies                        | Wastewater is absent (Tables 10 and 13)   |                        |
|   | $J_{B,P} = 0$ t/t   | $J_{B,A} = 0$ t/t      |

The reaction to obtain the sodium salt of 2-mercaptobenzothiazole is described by Scheme (5).

The formation of *N*-cyclohexyl-2-benzothiazolysulfenamide can be described by Scheme (6).

Based on the material balances calculated by us, we determined the consumption coefficients for raw materials and auxiliary materials (Table 12) and the waste generation

rates for the production of *N*-cyclohexyl-2-benzothiazolysulfenamide using an alternative technology (Table 13).

Next, we calculated comprehensive indicators for comparing the developed and alternative technologies used in the production of this product along with the final indicator for evaluating the developed technology for compliance with BAT principles (Table 14).

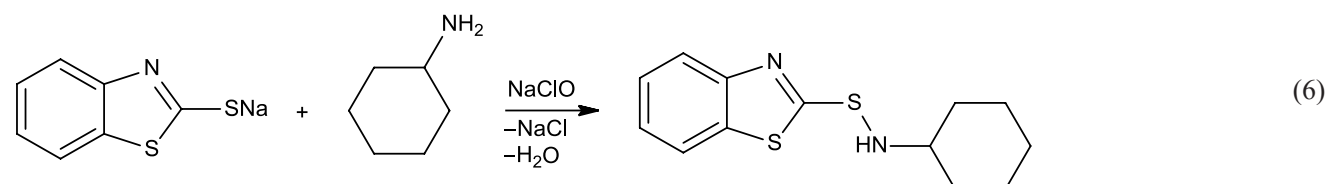
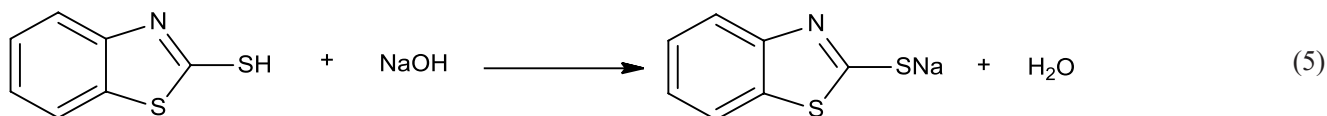


Table 12. Consumption coefficients for raw materials and auxiliary materials in the *N*-cyclohexyl-2-benzothiazolysulfenamide production using an alternative technology

| Name of raw materials          | Expense coefficients |      | Note                 |
|--------------------------------|----------------------|------|----------------------|
|                                | kg/operation         | t/t  |                      |
| 2-Mercaptobenzothiazole, 97%   | 68.80                | 0.73 | —                    |
| Sodium hydroxide, 44% solution | 44.46                | 0.47 | —                    |
| Water                          | 581.04               | 6.16 | Without regeneration |
|                                | 52.24                | 0.55 | With regeneration    |

Table 12. Continued

| Name of raw materials             | Expense coefficients |      | Note                 |
|-----------------------------------|----------------------|------|----------------------|
|                                   | kg/operation         | t/t  |                      |
| Cyclohexylamine, 99%              | 47.98                | 0.51 | Without regeneration |
|                                   | 40.12                | 0.42 | With regeneration    |
| Hydrochloric acid, 37% solution   | 51.30                | 0.54 | –                    |
| Sodium hypochlorite, 15% solution | 253.96               | 2.69 | –                    |
| Sodium sulfite                    | 14.69                | 0.16 | –                    |

Table 13. Waste generation standards, emissions, and discharges in the *N*-cyclohexyl-2-benzothiazolylsulfenamide production using an alternative technology (with water and cyclohexylamine regeneration)

| Production using an alternative technology (wastewater and by-product/mineral generation) |                          |                          |           |                                  |      |
|---|--------------------------|--------------------------|-----------|----------------------------------|------|
| Type of waste   | Aggregate state of waste | Composition              | Amount, % | Production waste generation rate |      |
|   |                          |                          |           | kg/operation                     | t/t  |
| Wastewater  | Liquid                   | VAT residue, including:  | 100.00    | 420.38                           | 4.45 |
|   |                          | Total organic impurities | 3.19      | 13.41                            | 0.14 |
|   |                          | Sodium chloride          | 14.47     | 60.84                            | 0.64 |
|   |                          | Sodium sulfate           | 3.94      | 16.56                            | 0.18 |
|   |                          | Water                    | 78.40     | 329.57                           | 3.49 |
| Air emissions   |                          | None                     |           |                                  |      |
| Wastewater discharge  |                          | None                     |           |                                  |      |

Table 14. Comprehensive indicators and the final evaluation of the developed technology for the production of *N*-cyclohexyl-2-benzothiazolylsulfenamide

| Indicator  | Calculation method and indicator value  |
|--|---|
| Comprehensive indicator of comparison of the main technological indicators of the developed and alternative technologies $K_1$   | <p>Due to the absence of emissions of harmful substances into the atmosphere or discharges of effluents into water bodies for the developed and alternative technologies, no comparison of specific indicators of such emissions into the atmosphere and discharges into water bodies is carried out.</p> $K_1 = (A_{T,P}/A_{T,A})/3$ $K_1 = (0.82/4.45)/3 = 0.06$  |
| Comprehensive indicator of comparison of additional technological indicators of the developed and alternative technologies $K_2$ | <p>Due to the absence of discharges into water bodies and emissions of harmful substances into the atmosphere for the developed and alternative technologies, no calculation or comparison of the degree of purification of discharges into water bodies and emissions of harmful substances into the atmosphere is carried out.</p> $K_2 = (J_{K,A}/J_{K,P} + J_{O,A}/J_{O,P})/4$ $K_2 = (1.64/1.71 + 0.55/0.93)/4 = 0.39$ |
| Technology assessment outcome $I$  | $I = 0.06 + 0.39 = 0.45$  |



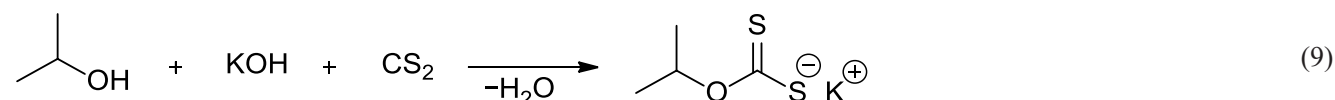
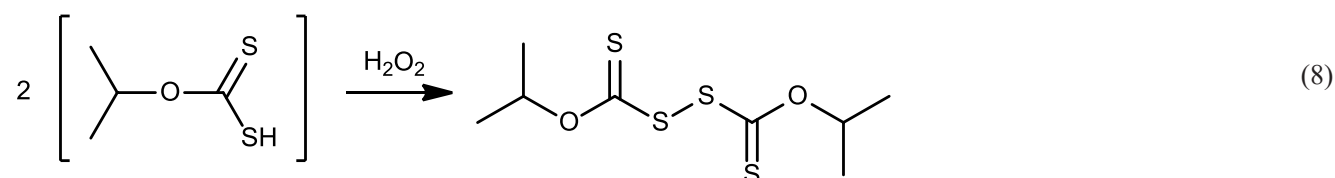
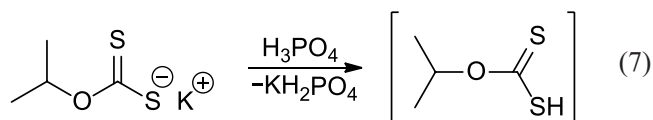
The value of the final indicator of technology assessment  $I = 0.45 \ll 2$  supports the conclusion that the technology developed by us for the production of *N*-cyclohexyl-2-benzothiazolylsulfenamide meets BAT principles and is much more environmentally friendly compared to the alternative [11] implemented in the USSR. This process has been introduced in aforementioned *Separate Plant No. 4*; the capacity of the pilot low-tonnage production is 5000 kg/year.

A distinctive feature of the technology developed by us for the production of *N*-cyclohexyl-2-benzothiazolylsulfenamide compared to that implemented earlier in the USSR is a significant reduction in the level of waste generation and a high degree of raw material recovery, which makes it possible to characterize the new technology as much more efficient ( $K_1 = 0.06$ ). The high level of environmental friendliness of the developed technology ( $K_2 = 0.39$ ) is ensured by minimizing losses due to high rates of resource saving (raw material conversion) and recovery of the solvent (water) and excess raw material component (cyclohexylamine).

#### Assessment of the compliance of the diisopropyl xanthogen disulfide production technology with the BAT principles

The technology for the production of diisopropyl xanthogen disulfide is based on the method published in [12], which includes the oxidation of potassium isopropyl xanthate (PIX) [13] with hydrogen peroxide in the presence of phosphoric acid in water [14]. The interaction of PIX with phosphoric acid with the formation of the corresponding xanthogenic acid is described by Scheme (7).

The oxidation of the obtained xanthogenic acid with hydrogen peroxide to form diisopropyl xanthogen disulfide is represented by Scheme (8).



The resulting suspension was filtered, washed with water and dried. Wash water was reused in the next synthesis as a solvent. PIX was obtained by the interaction of isopropanol, potassium hydroxide, and carbon disulfide according to Scheme (9).

The process was carried out in isopropanol at a molar ratio of isopropanol : carbon disulfide : potassium hydroxide equal to 7 : 1 : 1 and a temperature of 25–35°C. To restore the quality of alcohol, the method of two-stage distillation of the filtrate was used.

The calculation of the main and additional technological indicators of the production of diisopropyl xanthogen disulfide to assess the compliance of the technology with the principles of BAT was carried out using the data of the “Temporary process regulations for pilot low-tonnage production of potassium isopropyl xanthate, No. TTR-12-350” and “Temporary process regulations for pilot low-tonnage production of diisopropylxanthogendisulfide, No. TTR-13-350” on consumption coefficients for raw materials (Table 15) and the generation rate of production waste (Table 16). The results of calculating the main and additional technological indicators for the production of diisopropyl xanthogen disulfide using an alternative technology are presented in Table 17.

The final assessment of the developed technology for the production of diisopropyl xanthogen disulfide was carried out by comparing the developed technology with an alternative one based on the known method of its production by oxidation of alkali metal xanthate with sodium nitrite in the presence of mineral acids (HCl, H<sub>2</sub>SO<sub>4</sub>) [15]: one mole of acid is used to decompose sodium nitrite to nitrogen oxides, and the second mol—on the formation of xanthogenic acid from the corresponding salt. The liberated nitric oxide (IV) acts as an oxidizing agent in this process, which can be generally described by reaction Schemes (10)–(13):

**Table 15.** Consumption coefficients for raw materials and auxiliary materials in the production of diisopropyl xanthogen disulfide

| Name of raw materials                     | Expense coefficients |       | Note   |
|---|----------------------|-------|--|
|   | kg/operation         | t/t   |  |
| Obtaining PIX (98.88%)                    |                      |       |  |
| Isopropyl alcohol (99.59%)                | 416.16               | 2.593 | —  |
|   | 145.89               | 0.909 | With regeneration                            |
| Carbon disulfide (100%)                   | 72.68                | 0.453 | —  |
| Potassium hydroxide (86.11%)              | 61.70                | 0.384 | —  |
| Isopropanol recovery                      |                      |       |  |
| Toluene (99.5%)                           | 98.63                | 0.616 | —  |
| Obtaining diisopropyl xanthogen disulfide |                      |       |  |
| PIX (98.88%)                              | 150.00               | 1.42  | —  |
| Hydrogen peroxide (37%)                   | 43.56                | 0.41  | —  |
| Orthophosphoric acid (85%)                | 99.39                | 0.94  | —  |
| Water                                     | 850.00               | 8.03  | —  |
|   | 440.00               | 4.16  | Taking into account the return of wash water |

**Table 16.** Waste generation standards, emissions, and discharges in the diisopropyl xanthogen disulfide production (with isopropanol regeneration and return of washing water)

| Type of waste  | Aggregate state of waste | Composition             | Amount, % | Production waste generation rate |       |
|--|--------------------------|-------------------------|-----------|----------------------------------|-------|
|  |                          |                         |           | kg/operation                     | t/t   |
| VAT residue after rectification of the filtrate (stage of obtaining PIX) | Liquid                   | VAT residue, including: | 100.00    | 12.89                            | 0.086 |
|  |                          | Isopropanol             | 51.32     | 5.42                             | 0.039 |
|  |                          | Impurity                | 48.68     | 7.47                             | 0.047 |

Table 16. Continued

| Type of waste  | Aggregate state of waste | Composition             | Amount, % | Production waste generation rate |       |
|--|--------------------------|-------------------------|-----------|----------------------------------|-------|
|  |                          |                         |           | kg/operation                     | t/t   |
| Azeotrope isolated at the stage of rectified absolutization (stage of obtaining PIX) | Liquid                   | Azeotrope, including:   | 100.00    | 201.53                           | 1.260 |
|  |                          | Isopropanol             | 38.20     | 76.98                            | 0.481 |
|  |                          | Water                   | 13.10     | 26.40                            | 0.165 |
|  |                          | Toluene                 | 48.70     | 98.14                            | 0.613 |
| Distillation residue after absolute rectification (stage of obtaining PIX)           | Liquid                   | VAT residue, including: | 100.00    | 9.29                             | 0.021 |
|  |                          | Isopropanol             | 85.71     | 8.80                             | 0.018 |
|  |                          | Impurity                | 14.29     | 0.49                             | 0.003 |
| Wastewater (diisopropyl xanthogen disulfide production stage)                        | Liquid                   | Filtrate, including:    | 100.00    | 620.63                           | 5.862 |
|  |                          | Water                   | 79.03     | 490.47                           | 4.632 |
|  |                          | Impurity                | 20.97     | 130.16                           | 1.229 |
| Air emissions  | None                     |                         |           |                                  |       |
| Wastewater discharges  | None                     |                         |           |                                  |       |

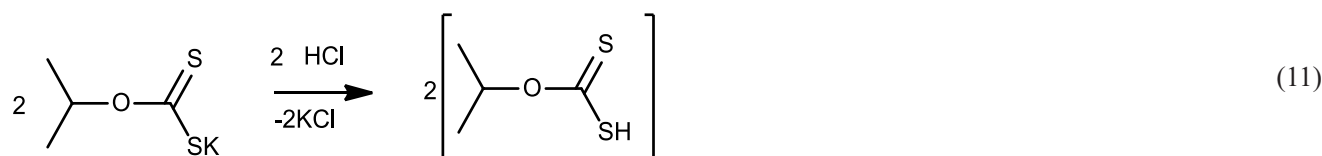
Table 17. Basic and additional technological indicators calculated for the developed and alternative technologies used in the diisopropyl xanthogen disulfide production

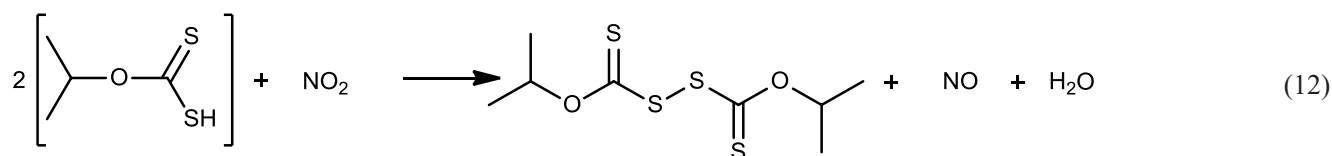
| Indicator                                 | Calculation method and indicator value  |  |
|---|---|--|
|   | Developed technology  | Alternative technology   |
| Main technological indicators             |   |  |
| Generation rate of solid and liquid waste | $A_{T,P} = 7.228 \text{ t/t}$ (Table 16)  | $A_{T,A} = 7.337 \text{ t/t}$ (Tables 20 and 21)   |
| Specific emissions into the atmosphere    | Process off-gases are water vapor. There are no emissions of harmful substances into the atmosphere (Table 16)<br>$B_{T,P} = 0 \text{ t/t}$ | Off-gases are a mixture of nitrogen and carbon dioxide. There are no emissions of harmful substances into the atmosphere (Tables 20 and 21)<br>$B_{T,A} = 0 \text{ t/t}$ |

Table 17. Continued

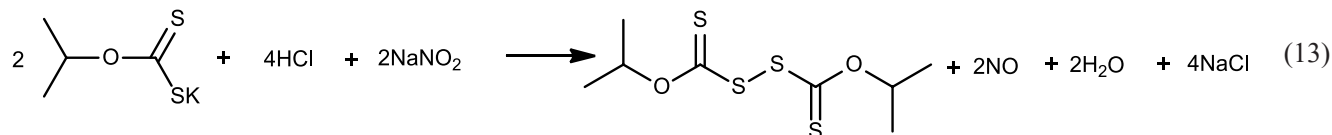
| Indicator   | Calculation method and indicator value   |   |
|---|--|---|
|   | Developed technology   | Alternative technology  |
| Wastewater generation rate  | There is no wastewater discharge due to the high hazard class for fishery water bodies (hazard class 2*). $C_{T,P} = 0$ t/t  | There is no wastewater discharge due to the high hazard class of the leachate for water bodies of fishery significance (hazard class 1*). $C_{T,A} = 0$ t/t   |
| Additional technological indicators   |  |   |
| The degree of complexity and completeness of the extraction of useful components from the feedstock | <p>It is calculated as the sum of the recovery factors for isopropanol <math>P_{IP}</math>, potassium hydroxide <math>P_{KOH}</math>, carbon disulfide <math>P_{CS_2}</math>, PIX <math>P_{PIX}</math>, hydrogen peroxide <math>P_{H_2O_2}</math>, and phosphoric acid <math>P_{H_3PO_4}</math> taking into account the yield of diisopropylxanthogendisulfide (105.88 kg per operation, 90%).</p> $P_{IP} = 0.341/0.358 = 0.95 \text{ t/t}$ $P_{KOH} = 0.319/0.334 = 0.95 \text{ t/t}$ $P_{CS_2} = 0.433/0.453 = 0.95 \text{ t/t}$ $P_{PIX} = 1.261/1.401 = 0.90 \text{ t/t}$ <p>Taking into account the degree of extraction of the components of the PIX production process:</p> $P_{PIX} = 0.95 \times 0.90 = 0.86 \text{ t/t}$ $P_{H_2O_2} = 0.123/0.152 = 0.81 \text{ t/t}$ $P_{H_3PO_4} = 0.713/0.798 = 0.89 \text{ t/t}$ $J_{K,P} = 0.86 + 0.81 + 0.89 = 2.56 \text{ t/t}$ | <p>Recovery factors for carbon disulfide <math>P_{CS_2}</math>, isopropanol <math>P_{IP}</math>, potassium hydroxide <math>P_{KOH}</math> for the stage of obtaining PIX:</p> $P_{IP} = 0.341/0.358 = 0.95 \text{ t/t}$ $P_{KOH} = 0.319/0.334 = 0.95 \text{ t/t}$ $P_{CS_2} = 0.433/0.453 = 0.95 \text{ t/t}$ <p>Recovery factors of PIX, sodium nitrite <math>P_{NaNO_2}</math>, and phosphoric acid <math>P_{H_3PO_4}</math> taking into account the yield of the product (108.25 kg per operation, 94.1%).</p> $P_{PIX} = 0.95 \times 0.94 = 0.89 \text{ t/t}$ $P_{NaNO_2} = 0.44/0.47 = 0.94 \text{ t/t}$ $P_{H_3PO_4} = 0.611/0.611 = 1.00 \text{ t/t}$ $J_{K,A} = 0.89 + 0.94 + 1.00 = 2.83 \text{ t/t}$ |
| Degree of utilization of generated waste  | <p>It is calculated as the share of regenerated isopropanol in the total mass of waste (filtrate and condensate). According to the material balance of isopropanol regeneration per 1 t of product:</p> $J_{O,P} = (0.984 + 0.700)/3.049 = 0.55 \text{ t/t}$   | <p>It is calculated as the share of returned water in the total mass of waste (filtrate, wash water and waste absorbent). According to the material balance per 1 t of product:</p> $J_{O,A} = 4.610/9.772 = 0.47 \text{ t/t}$  |
| Degree of purification of emissions of harmful substances into the atmosphere                       | <p>Process off-gases are water vapor. There are no emissions of harmful substances into the atmosphere.</p> $J_{A,P} = 1.00 \text{ t/t}$   | <p>It is calculated as the share of captured nitrogen oxide in the total mass of off-gases:</p> $J_{A,A} = 0.030/0.030 = 1.00 \text{ t/t}$  |
| Degree of purification of discharges into water bodies  | There is no wastewater discharge (Tables 16, 20, and 21)   |   |
|   | $J_{B,P} = 0$ t/t  | $J_{B,A} = 0$ t/t   |

\* Order of the Ministry of Natural Resources of Russia dated December 4, 2014 No. 536 "On approval of the criteria for classifying wastes as hazard classes I–V according to the degree of negative impact on the environment" (Registered in the Ministry of Justice of Russia on December 29, 2015, No. 40330).

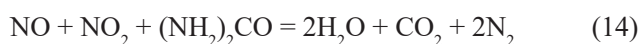




In total:



Purification of gas emissions is carried out by absorption of off-gases with an aqueous solution of urea. The process of absorption of nitrogen oxides can be described by Scheme (14):



Based on the calculated by us material balances, the consumption coefficients for raw materials and auxiliary materials (Tables 18 and 19) and the waste generation rate in the production of diisopropyl xanthogen disulfide using an alternative technology were determined (Tables 20 and 21).

**Table 18.** Consumption coefficients for raw materials and auxiliary materials in the potassium isopropyl xanthate production

| Name of raw materials       | Expense coefficients |       | Note              |
|-----------------------------|----------------------|-------|-------------------|
|                             | kg/operation         | t/t   |                   |
| Obtaining PIX               |                      |       |                   |
| Isopropyl alcohol (99.6%)   | 416.16               | 2.593 | –                 |
|                             | 145.89               | 0.909 | With regeneration |
| Carbon disulfide (100%)     | 72.68                | 0.453 | –                 |
| Potassium hydroxide (86.8%) | 61.70                | 0.384 | –                 |
| Isopropanol recovery        |                      |       |                   |
| Toluene (99.5%)             | 98.63                | 0.616 | –                 |

**Table 19.** Consumption coefficients for raw materials and auxiliary materials in the diisopropyl xanthogen disulfide production using an alternative technology

| Name of raw materials      | Expense coefficients |       | Note |
|----------------------------|----------------------|-------|------|
|                            | kg/operation         | t/t   |      |
| PIX (98.88%)               | 150.00               | 1.355 | –    |
| Sodium nitrite (98.50%)    | 59.60                | 0.552 | –    |
| Orthophosphoric acid (85%) | 127.10               | 1.196 | –    |

Table 19. Continued

| Name of raw materials            | Expense coefficients |       | Note  |
|----------------------------------|----------------------|-------|---|
|                                  | kg/operation         | t/t   |   |
| Water                            | 850.00               | 7.870 | —   |
|                                  | 433.86               | 4.017 | With the return of wash water and condensate from the sludge drying process |
| Urea (100%)*                     | 133.02*              | 0.172 | With recycling  |
|                                  | 121.63*              | 0.157 | With the regeneration of the absorbent                                      |
| Water for absorbent preparation* | 399.06*              | 0.515 | With recycling  |

\* Based on 7 operations for obtaining diisopropyl xanthogen disulfide.

Table 20. Waste generation standards, emissions, and discharges in the potassium isopropyl xanthate production

| Type of waste   | Aggregate state of waste | Composition             | Amount, % | Production waste generation rate |       |
|---|--------------------------|-------------------------|-----------|----------------------------------|-------|
|   |                          |                         |           | kg/operation                     | t/t   |
| VAT residue after distillation of the filtrate            | Liquid                   | VAT residue, including: | 100.00    | 12.89                            | 0.086 |
|   |                          | Isopropanol             | 51.32     | 5.42                             | 0.039 |
|   |                          | Impurities              | 48.68     | 7.47                             | 0.047 |
| Azeotrope isolated at the stage of absolute rectification | Liquid                   | Azeotrope, including:   | 100.00    | 201.53                           | 1.260 |
|   |                          | Isopropanol             | 38.20     | 76.98                            | 0.481 |
|   |                          | Water                   | 13.10     | 26.40                            | 0.165 |
|   |                          | Toluene                 | 48.70     | 98.14                            | 0.613 |
| Distillation residue after absolute rectification         | Liquid                   | VAT residue, including: | 100.00    | 9.29                             | 0.021 |
|   |                          | Isopropanol             | 85.71     | 8.80                             | 0.018 |
|   |                          | Impurities              | 14.29     | 0.49                             | 0.003 |
| Air emissions   |                          | None                    |           |                                  |       |
| Wastewater discharges                                     |                          | None                    |           |                                  |       |



**Table 21.** Waste generation standards, emissions, and discharges in the diisopropyl xanthogen disulfide production using an alternative technology

| Type of waste         | Aggregate state of waste | Composition                                   | Amount, % | Production waste generation rate |       |
|-----------------------|--------------------------|---|-----------|----------------------------------|-------|
|                       |                          |   |           | kg/operation                     | t/t   |
| Wastewater            | Liquid                   | Filtrate, including:                          | 100.00    | 629.60                           | 5.830 |
|                       |                          | Water   | 74.13     | 466.72                           | 4.321 |
|                       |                          | Impurities                                    | 1.25      | 7.87                             | 0.073 |
|                       |                          | Sodium and potassium salts of phosphoric acid | 24.62     | 155.01                           | 1.435 |
| Wastewater            | Liquid                   | Waste absorbent, including:                   | 100.00    | 15.45                            | 0.140 |
|                       |                          | Urea  | 2.78      | 0.43                             | 0.004 |
|                       |                          | Water   | 97.22     | 15.02                            | 0.136 |
| Abgases               | Gas                      | Abgases, including                            | 100.00    | 13.82                            | 0.125 |
|                       |                          | Nitrogen                                      | 10.34     | 1.43                             | 0.013 |
|                       |                          | Carbon dioxide                                | 89.66     | 12.39                            | 0.112 |
| Air emissions         |                          | None  |           |                                  |       |
| Wastewater discharges |                          | None  |           |                                  |       |

Further, we calculated the comprehensive indicators for comparing the developed and alternative technologies used in the production of diisopropyl xanthogen disulfide along with the final indicator for evaluating the developed technology for compliance with BAT principles (Table 22).

The value of the final indicator of the technology assessment  $I = 1.97 < 2$  supports the conclusion that the technology developed by us for the production of diisopropyl xanthogen disulfide meets BAT principles and is more environmentally friendly compared to the alternative one [4]. This technology was introduced in *Separate Plant No. 4*; the capacity of the pilot low-scale production is 2000 kg/year for diisopropyl xanthogen disulfide and 3000 kg/year for PIX.

Thus, the developed technology is more environmentally friendly than the alternative one due to the high level of environmental friendliness achieved through the regeneration of isopropanol at the stage of PIX production. However, the specific indicator of waste generation by this technology is quite high (7.23 t/t, Table 17), and the main production waste is the filtrate from the stage of obtaining diisopropyl xanthogen disulfide (5.862 t/t, Table 21), the water content of which is 79.03%. It should be noted that during the development process, we managed to reduce the hazard class of this waste from 1st to 2nd, which, in our opinion, is a significant result in achieving environmental protection goals and increases the level of environmental friendliness of the technology we developed for the production of diisopropyl

<sup>6</sup> Order of the Ministry of Agriculture of Russia dated December 13, 2016, No. 552 (as amended on March 10, 2020) "On approval of water quality standards for fishery water bodies, including standards for maximum permissible concentrations of harmful substances in the waters of fishery water bodies" (Registered with the Ministry of Justice of Russia on January 13, 2017, No. 45203) (in Russ.).

**Table 22.** Comprehensive indicators and the final evaluation indicator of the developed diisopropyl xanthogen disulfide production technology

| Indicator  | Calculation method and indicator value   |
|--|--|
| Comprehensive indicator of comparison of the main technological indicators of the developed and alternative technologies $K_1$   | Due to the absence of emissions of harmful substances into the atmosphere or discharges into water bodies for these technologies, no comparison of specific indicators of emissions into the atmosphere and discharges into water bodies is carried out.<br>$K_1 = A_{T,P}/A_{T,A} = 7.23/7.34 = 0.98$ |
| Comprehensive indicator of comparison of additional technological indicators of the developed and alternative technologies $K_2$ | Due to the absence of discharges of harmful substances into water bodies using these technologies, no calculation or comparison of the degree of purification of discharges into water bodies is carried out.<br>$K_2 = (2.83/2.56 + 0.47/0.55 + 1.00/1.00)/3 = (1.11 + 0.85 + 1.00)/3 = 0.99$         |
| Technology assessment outcome $I$  | $I = 0.98 + 0.99 = 1.97$   |

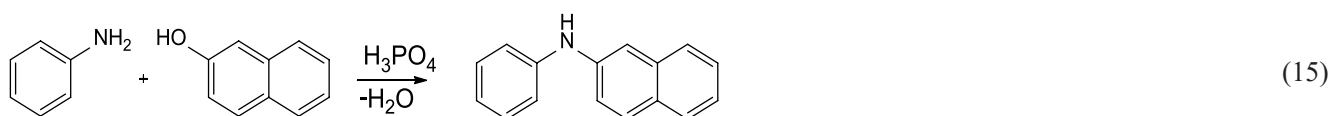
xanthogen disulfide. Regeneration of the solvent (water) from the waste (filtrate) can be considered as a possible direction for the modernization of the technology, which will lead to a decrease in the specific indicator of production waste and will increase the degree of use of raw materials and generated waste.

#### Assessment of the compliance of the developed technology for the *N*-phenyl-2-naphthylamine production with the BAT principles

The technology for the production of *N*-phenyl-2-naphthylamine was based on a one-stage method developed in [16], which includes the amination of 2-naphthol with aniline in the presence of catalytic amounts of orthophosphoric acid at a molar ratio

of 2-naphthol : aniline : orthophosphoric acid equal to 1 : 1.065 : 0.017, within 2.0–2.5 h [17, 18]. The return of the initial aniline to the reaction sphere is ensured by separating the azeotropic aniline/water mixture and separating *N*-phenyl-2-naphthylamine in the form of a powder by crystallization from the reaction mass in an isobutanol/xylene mixture [16, 17]. The process of obtaining *N*-phenyl-2-naphthylamine is described by Scheme (15).

The calculation of the main and additional technological indicators [4] of the production of *N*-phenyl-2-naphthylamine was carried out by us using data of “Temporary process regulations for pilot low-tonnage production of *N*-phenyl-2-naphthylamine, No. TTR-8-350” on consumption coefficients for raw materials (Table 23) and

**Table 23.** Consumption coefficients for raw materials and auxiliary materials in the *N*-phenyl-2-naphthylamine production

| Name of raw materials    | Expense coefficients |       | Note                 |
|--------------------------|----------------------|-------|----------------------|
|                          | kg/operation         | t/t   |                      |
| Aniline (99.9%)          | 121.00               | 0.475 | –                    |
| 2-Naphthol (99.5%)       | 175.00               | 0.686 | –                    |
| Phosphoric acid (85%)    | 2.40                 | 0.009 | –                    |
| Isobutanol (99.3%)       | 433.42               | 1.700 | Without regeneration |
|                          | 1.90                 | 0.007 | With regeneration    |
| Petroleum xylene (99.6%) | 82.91                | 0.325 | Without regeneration |
|                          | 32.27                | 0.127 | With regeneration    |

production waste generation rates (Table 24). The results of the calculation of the main and additional technological indicators are presented in Table 25.

The final assessment of the developed technology for the *N*-phenyl-2-naphthylamine production was also carried out by comparing this technology with an alternative one, which was

implemented in the 1960s at *Novomoskovsk Anilino-Paint Plant (Novomoskovsk Organic Synthesis Plant)* [19]. The technology was based on the condensation of 2-naphthol with aniline in the presence of a benzenesulfonic acid catalyst at a molar ratio of 2-naphthol to aniline equal to 1 : 1.5. The process of formation of *N*-phenyl-2-naphthylamine can be described by the Scheme (16).

**Table 24.** Waste generation standards, emissions, and discharges in the *N*-phenyl-2-naphthylamine production (with regeneration of isobutanol-*o*-xylene mixture)

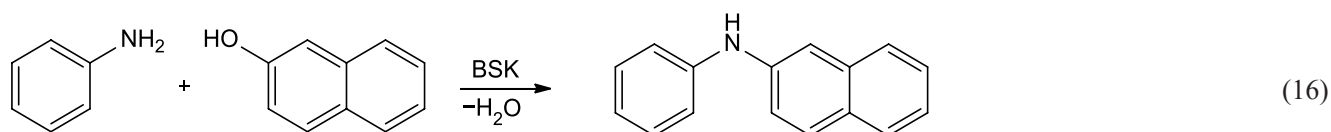
| Type of waste   | Aggregate state of waste | Composition                      | Amount, % | Production waste generation rate |       |
|---|--------------------------|----------------------------------|-----------|----------------------------------|-------|
|   |                          |                                  |           | kg/operation                     | t/t   |
| Distillation residue after regeneration of isobutanol- <i>o</i> -xylene mixture | Liquid                   | VAT residue, including:          | 100.00    | 54.23                            | 0.213 |
|   |                          | <i>N</i> -phenyl-2-naphthylamine | 8.32      | 10.03                            | 0.039 |
|   |                          | Aniline phosphate                | 3.30      | 3.98                             | 0.016 |
|   |                          | <i>o</i> -Xylene                 | 81.07     | 31.90                            | 0.125 |
|   |                          | Aniline                          | 5.09      | 6.14                             | 0.024 |
|   |                          | Impurities                       | 1.14      | 2.18                             | 0.009 |
| Aqueous phase (azeotrope)   | Liquid                   | Water                            | 100.00    | 22.15                            | 0.087 |
| Organic phase (azeotrope)   | Liquid                   | Organic phase, including:        | 100.00    | 2.61                             | 0.010 |
|   |                          | Aniline                          | 13.08     | 0.34                             | 0.001 |
|   |                          | Isobutanol                       | 70.11     | 1.90                             | 0.007 |
|   |                          | Xylene                           | 16.81     | 0.37                             | 0.001 |
| Air emissions   | None                     |                                  |           |                                  |       |
| Wastewater discharges   | None                     |                                  |           |                                  |       |

**Table 25.** Basic and additional technological indicators calculated for the developed and alternative technologies used in the *N*-phenyl-2-naphthylamine production

| Indicator                                 | Calculation method and indicator value                        |   |
|---|---|---|
|   | Developed technology  | Alternative technology                  |
| Main technological indicators             |   |   |
| Generation rate of solid and liquid waste | $A_{T,P} = 0.310 \text{ t/t}$ (Table 24)                      | $A_{T,P} = 1.85 \text{ t/t}$ (Table 27) |
| Specific emissions into the atmosphere    | There are no emissions into the atmosphere (Tables 24 and 27) |   |
|   | $B_{T,P} = 0 \text{ t/t}$                                     | $B_{T,A} = 0 \text{ t/t}$               |

Table 25. Continued

| Indicator   | Calculation method and indicator value   |                              |
|---|--|------------------------------|
|   | Developed technology   | Alternative technology       |
| Wastewater generation rate  | There is no wastewater discharge (Tables 24 and 27)  |                              |
|   | $C_{T,P} = 0 \text{ t/t}$  | $C_{T,A} = 0 \text{ t/t}$    |
| Additional technological indicators   |  |                              |
| The degree of complexity and completeness of the extraction of useful components from the feedstock | It is calculated as the sum of the recovery factors of 2-naphthol and aniline, taking into account the yield of <i>N</i> -phenyl-2-naphthylamine (255.00 kg per operation, 96%)<br>$P_{2\text{-Naphthol}} = 0.659/0.683 = 0.96 \text{ t/t}$<br>$P_{\text{Aniline}} = 0.424/0.474 = 0.89 \text{ t/t}$<br>$J_{K,P} = 0.96 + 0.89 = 1.85 \text{ t/t}$ | $J_{K,A} = 1.59 \text{ t/t}$ |
| Degree of utilization of generated waste  | It is calculated as the share of regenerated isobutanol and xylene in the total mass of the waste (filtrate, washing solution, and condensate). It can be calculated from the material balance data for the regeneration of the isobutanol/xylene mixture per operation.<br>$J_{O,P} = (431.47 + 50.60)/538.39 = 0.90 \text{ t/t}$                 | $J_{O,A} = 0.31 \text{ t/t}$ |
| Degree of purification of emissions of harmful substances into the atmosphere                       | There are no emissions into the atmosphere (Tables 24 and 27)  |                              |
|   | $J_{A,P} = 0 \text{ t/t}$  | $J_{A,A} = 0 \text{ t/t}$    |
| Degree of purification of discharges into water bodies  | There is no wastewater discharge (Tables 24 and 27)  |                              |
|   | $J_{B,P} = 0 \text{ t/t}$  | $J_{B,A} = 0 \text{ t/t}$    |



The condensation of 2-naphthol and aniline was carried out at a temperature of  $240 \pm 5^\circ\text{C}$  until the content of 2-naphthol was 0.8%. Aniline vapor was partially returned to the reactor by reflux. The reaction mass was neutralized with solid caustic soda. Unreacted aniline was distilled off with live steam until it was completely absent in the reaction mass. The selection of the target *N*-phenyl-2-naphthylamine was carried out in the form of a melt, followed by distillation and flaking.

Regeneration of excess aniline that did not react with 2-naphthol was carried out using vacuum distillation and rectification methods. The extraction

of aniline from aniline water was carried out in the process of rectification by azeotropic distillation, followed by separation of the heteroazeotrope by centrifugation.

Based on the calculated by us material balances, the consumption coefficients for raw materials and auxiliary materials (Table 26) and the generation rate of *N*-phenyl-2-naphthylamine production waste using an alternative technology were determined (Table 27).

Next, we calculated comprehensive indicators for comparing the developed and alternative technologies and the final indicator for evaluating the new technology for compliance with BAT principles (Table 28)

**Table 26.** Consumption coefficients for raw materials and auxiliary materials in the *N*-phenyl-2-naphthylamine production using an alternative technology

| Name of raw materials              | Expense coefficients |       | Note                 |
|------------------------------------|----------------------|-------|----------------------|
|                                    | kg/operation         | t/t   |                      |
| Technical aniline (99.8%)          | 1854.55              | 0.663 | Without regeneration |
|                                    | 1185.99              | 0.424 | With regeneration    |
| 2-Naphthol (98.5%)                 | 1940.00              | 0.693 | –                    |
| Benzenesulfonic acid (95%)         | 8.90                 | 0.003 | –                    |
| Technical sodium hydroxide (98.5%) | 2.30                 | 0.001 | –                    |
| Water                              | 3500.00              | 1.250 | Without regeneration |
|                                    | 2659.57              | 0.950 | With regeneration    |
| Water vapor                        | 2238.24              | 0.800 | –                    |

**Table 27.** Waste generation standards, emissions, and discharges in the *N*-phenyl-2-naphthylamine production using an alternative technology (with water and aniline regeneration)

| Type of waste         | Aggregate state of waste | Composition                         | Amount, % | Production waste generation rate |         |
|-----------------------|--------------------------|-------------------------------------|-----------|----------------------------------|---------|
|                       |                          |                                     |           | kg/operation                     | t/t     |
| Wastewater            | Liquid                   | Filtrate, including:                | 100.00    | 121.099                          | 0.433   |
|                       |                          | 2-Naphthol                          | 0.09      | 0.114                            | 0.0004  |
|                       |                          | Sodium salt of benzenesulfonic acid | 0.60      | 0.722                            | 0.0026  |
|                       |                          | Sodium salt of sulfuric acid        | 0.02      | 0.029                            | 0.0001  |
|                       |                          | Water                               | 95.06     | 115.117                          | 0.4113  |
|                       |                          | Impurities                          | 4.23      | 5.118                            | 0.0183  |
| Wastewater            | Liquid                   | Wash water, including:              | 100.00    | 255.532                          | 0.913   |
|                       |                          | 2-Naphthol                          | 0.09      | 0.222                            | 0.0008  |
|                       |                          | Sodium salt of benzenesulfonic acid | 0.09      | 0.241                            | 0.0009  |
|                       |                          | Sodium salt of sulfuric acid        | 0.004     | 0.010                            | 0.00004 |
|                       |                          | Water                               | 99.31     | 253.779                          | 0.9067  |
|                       |                          | Impurities                          | 0.50      | 1.280                            | 0.0046  |
| VAT residue           | Liquid                   | VAT residue, including:             | 100.00    | 0.400                            | 0.001   |
|                       |                          | Resin                               | 100.00    | 0.400                            | 0.001   |
| Wastewater            | Liquid                   | Water, including:                   | 100.00    | 141.110                          | 0.504   |
|                       |                          | Aniline                             | 0.15      | 0.210                            | 0.0008  |
|                       |                          | Water                               | 99.85     | 140.900                          | 0.5034  |
| Air emissions         |                          | None                                |           |                                  |         |
| Wastewater discharges |                          | None                                |           |                                  |         |

**Table 28.** Comprehensive indicators and the final evaluation indicator of the developed *N*-phenyl-2-naphthylamine production technology

| Indicator  | Calculation method and indicator value  |
|--|---|
| Comprehensive indicator of comparison of the main technological indicators of the developed and alternative technologies $K_1$   | <p>Due to the absence of emissions of harmful substances into the atmosphere or discharges into water bodies for the technologies under consideration, the formula for calculating the indicator is transformed as follows:</p> $K_1 = A_{T,P}/A_{T,A}$ $K_1 = 0.31/1.85 = 0.17$  |
| Comprehensive indicator of comparison of additional technological indicators of the developed and alternative technologies $K_2$ | <p>Due to the absence of emissions of harmful substances into the atmosphere for the technologies under consideration, no calculation or comparison of the degree of purification of emissions of harmful substances into the atmosphere is carried out.</p> $K_2 = (J_{K,A}/J_{K,P} + J_{O,A}/J_{O,P} + J_{B,A}/J_{B,P})/3$ $K_2 = (1.59/1.85 + 0.31/0.90 + 1.00/1.00)/3 = 0.73$ |
| Technology assessment outcome $I$  | $I = 0.17 + 0.73 = 0.90$  |

The value of the final technology assessment indicator  $I = 0.90 \ll 2$  supports the conclusion that the *N*-phenyl-2-naphthylamine production technology developed by us meets BAT principles and is much more environmentally friendly [4] compared to the alternative one implemented in the USSR. The technology developed by us has been implemented in *Separate Plant No. 4*; the capacity of the experimental low-tonnage production is 5000 kg/year.

An analysis of the evaluation of the developed *N*-phenyl-2-naphthylamine production technology determines it as highly efficient ( $K_1 = 0.17$ ) and having a high level of environmental friendliness ( $K_2 = 0.73$ ). The new technology is distinguished by a significantly lower (almost 6 times) level of waste generation compared to the alternative technology implemented in the USSR, and is also characterized by a high degree of resource saving and recuperation of generated waste. The obtained result is ensured by the adopted technological solutions using the return of aniline to the reaction sphere after the separation of the condensed in florentine vapors of the azeotropic aniline–water mixture, as well as the regeneration of the mixture of solvents (isobutanol/xylene).

## DISCUSSION

Based on the analysis of new low-tonnage chemical production technologies developed at *GosNIIOKhT* according to the criteria for achieving environmental protection objectives using the methodology [4], the adopted technological solutions for resource saving and environmental protection are concluded to be highly effective.

The quantitative assessment methodology [4] is based on determining achieved levels of manufacturability and environmental friendliness of new technologies along with the calculation of comprehensive indicator for comparison with alternative (BAT) technologies (Table 29). The calculated values of the main technological indicators characterize the achieved level of technology efficiency: the lower the value of the  $K_1$  indicator, the higher the efficiency of the new technology compared to the existing alternative. In turn, the values of additional technological indicators of technologies reflect the achieved level of environmental friendliness of the technology, while the criterion for the effectiveness of the development (compared to the existing technology) also consists in the achievement of the minimum values of the  $K_2$  indicator. The effectiveness of development as a whole characterizes the final indicator of comparison  $I$ : the lower its value, the higher the achieved degree of compliance of the new technology with BAT principles and the current level of development according to the criteria for achieving the environmental protection objectives.

The current absence of BAT for the production of tetramethylthiuram disulfide (thiuram D), *N*-cyclohexyl-2-benzothiazolylsulfenamide (sulfenamide C), diisopropyl xanthogen disulfide (diproxide) and *N*-phenyl-2-naphthylamine (neozone D) is due to these materials having previously been produced in the USSR.

As a result of the calculations, it was found that all the new technologies developed by us in accordance with BAT principles are environmentally more advanced than those implemented earlier during the Soviet period (Table 30). The most



**Table 29.** Criteria for the development and evaluation indicators of new technologies in accordance with BAT principles

| Criteria for development in accordance with BAT principles | Evaluation indicators for developed and alternative production technologies in accordance with BAT principles                                      |  |  |
|--|--|--|--|
|  | $K_1$ (achieved level of technology efficiency)  | $K_2$ (achieved level environmental friendliness of the technology)  | $I$ (overall development efficiency)   |
| Development efficiency criterion                           | $K_1 < 1$<br>Reaching the minimum values of $K_1$  | $K_2 < 1$<br>Reaching the minimum values of $K_2$  | $I < 2$<br>Reaching the minimum values of $I$  |
| Characteristics of development evaluation indicators       | Comprehensive indicator of comparison of the main technological indicators of production technologies  | Comprehensive indicator of comparison of additional technological indicators of the developed and alternative production technologies  | Final indicator of the comparison of the developed and alternative production technologies   |
| Semantic content of development evaluation indicators      | Level of waste generation, air emissions and water discharges.   | Degree of complexity and completeness of the extraction of useful components from the feedstock, the use of waste generated, the purification of emissions of harmful substances into the atmosphere and discharges into water bodies. | Degree of compliance of the new technology with BAT principles and the current level of development according to the criteria for achieving the objectives of environmental protection |
| Conclusion on the results of the development evaluation    | $K_1 < 1$ .<br>The lower the $K_1$ indicator, the higher the achieved level of efficiency of the developed technology compared to the alternative. | $K_2 < 1$ .<br>The lower the $K_2$ indicator, the higher the achieved level of environmental friendliness of the developed technology compared to the alternative.   | $I < 2$ .<br>The lower $I$ , the more the developed technology complies with BAT principles and is more environmentally friendly compared to the alternative.                          |

**Table 30.** Results of the quantitative assessment of the developed technologies for the production of materials in accordance with BAT principles

| Development evaluation indicators in accordance with BAT principles | Subject of development—production technology |  |                                 |                                  |
|---|--|--|---------------------------------|----------------------------------|
|   | Tetramethylthiuram disulfide                 | <i>N</i> -cyclohexyl-2-benzothiazolylsulfenamide | Diisopropyl xanthogen disulfide | <i>N</i> -phenyl-2-naphthylamine |

Development evaluation results

|       |      |      |      |      |
|-------|------|------|------|------|
| $K_1$ | 0.11 | 0.06 | 0.98 | 0.17 |
| $K_2$ | 0.93 | 0.39 | 0.99 | 0.73 |
| $I$   | 1.04 | 0.45 | 1.97 | 0.90 |

Table 30. Continued

| Development evaluation indicators in accordance with BAT principles | Subject of development—production technology                             |  |   |                                  |
|---|--|--|---|----------------------------------|
|   | Tetramethylthiuram disulfide   | <i>N</i> -cyclohexyl-2-benzothiazolylsulfenamide | Diisopropyl xanthogen disulfide                               | <i>N</i> -phenyl-2-naphthylamine |
| Conclusion on the results of the development evaluation:            |  |  |   |                                  |
| Achieved level of efficiency  | Very high  | Very high  | Comparable  | Very high                        |
| Achieved level of environmental friendliness                        | Comparable   | Very high  | Comparable  | High                             |
| Overall development efficiency                                      | Very high  | Very high  | Comparable  | Very high                        |
| Compliance with BAT principles                                      | Yes  | Yes  | Yes   | Yes                              |
| Identification of possible directions for development modernization |  |  |   |                                  |
| Possible modernization measures                                     | Regeneration of water from waste (leachate)                              | —  | Solvent (water) recovery from waste (filtrate)                | —                                |
| Expected result of modernization measures                           | Reducing the specific indicator of production waste                      | —  | Reducing the specific indicator of production waste           | —                                |
|   | Increasing the utilization of generated waste                            | —  | Increasing the utilization of generated waste                 | —                                |
|   | Further improvement of the environmental friendliness of the development | —  | Further increase in efficiency and environmental friendliness | —                                |

effective technological solutions have been developed for the production of tetramethylthiuram disulfide ( $K_1 = 0.11 \ll 1$ ), *N*-cyclohexyl-2-benzothiazolylsulfenamide ( $K_1 = 0.06 \ll 1$ ) and *N*-phenyl-2-naphthylamine ( $K_1 = 0.17 \ll 1$ ). The maximally efficient use of raw materials and purification of emissions and discharges is achieved by implementing the technologies for the production of *N*-cyclohexyl-2-benzothiazolylsulfenamide ( $K_2 = 0.39 < 1$ ) and *N*-phenyl-2-naphthylamine ( $K_1 = 0.73 < 1$ ). The achieved levels of manufacturability ( $K_1$ ) and environmental friendliness ( $K_2$ ) provide a high level of efficiency and compliance with BAT principles for the production of tetramethylthiuram disulfide ( $I = 1.04 \ll 2$ ),

*N*-cyclohexyl-2-benzothiazolylsulfenamide ( $I = 0.45 \ll 2$ ) and *N*-phenyl-2-naphthylamine ( $I = 0.9 \ll 2$ ).

The developed new technology for the production of diisopropyl xanthogen disulfide is characterized by the levels of manufacturability ( $K_1 = 0.98 \approx 1$ ) and environmental friendliness ( $K_2 = 0.99 \approx 1$ ) comparable with the alternative option. The efficiency of the developed technological solutions is also comparable with the efficiency of the alternative ( $I = 1.97$ ). Nevertheless, compliance with the development efficiency criterion ( $I = 1.97 < 2$ ) supports the conclusion that the new technology offers some advantage in terms of achieved resource saving and environmental protection in accordance with BAT principles.

A possible direction for the modernization of this development consists in the search for new technological solutions for the recovery of a solvent (water) from waste (filtrate), which will increase its efficiency and environmental friendliness by reducing the specific indicator of waste production and enhancing the utility of generated wastes.

## CONCLUSIONS

The introduction of modern low-tonnage chemical production technologies on an industrial scale is a complex system task, whose successful solution is ensured by the achievement of high levels of efficiency, safety and quality of development. Decisions on the prospects for industrial implementation of possible new technologies should be made based on the results of their analysis according to criteria for determining the result achieved during implementation, as well as compliance with regulatory and legislative requirements. An objective assessment must have a scientific methodological basis that takes technological, economic and environmental factors into account, as well as an algorithm for evaluating achieved indicators, comparing them with the target ones, and drawing a conclusion about the level of development.

To assess the compliance of new technologies with modern environmental requirements, we have developed a "Methodology for the quantitative assessment of new technologies for the production of organic substances in accordance with BAT principles," which is used in the development process to make decisions on resource saving and waste reduction.

On the example of low-tonnage technologies for the production of tetramethylthiuram disulfide, *N*-cyclohexyl-2-benzothiazolylsulfenamide, diisopropyl xanthogen disulfide and *N*-phenyl-2-naphthylamine created at *GosNIIOKhT*, the quantitative assessment of new technologies based on the calculation of comprehensive indicators of comparison with alternative technologies by technological (quantity waste, emissions and discharges) and environmental indicators (the degree of use of raw materials and

waste and the effectiveness of measures to clean up gas emissions and discharges into water bodies) is shown to be useful for assessing the compliance of new technologies with BAT principles, as well as determining the directions for modernizing existing industries.

The developed "Methodology for a comprehensive assessment of possible technological solutions according to the criteria of economic and environmental efficiency," along with the "Methodology for the quantitative assessment of new technologies for the production of materials in accordance with BAT principles" allowed us to create a methodological basis for use at the stage of making basic technological decisions on the introduced production method to ensure a high level of economic and environmental efficiency, as well as fulfilling legal requirements for technologies used in the field of environmental safety for achieving environmental protection objectives.

### Authors' contributions

**N.A. Kostikova** – development and industrial implementation of technologies for the production of tetramethylthiuram disulfide, *N*-cyclohexyl-2-benzothiazolylsulfenamide, diisopropyl xanthogen disulfide, and *N*-phenyl-2-naphthylamine; development of the "Methodology for the quantitative assessment of new technologies for the production of organic substances in accordance with BAT principles," approbation of this technique, and the comparative evaluation of developed and alternative (previously implemented in the USSR) technologies by the level of environmental impact.

**E.N. Glukhan** – formation of the scientific concept of quantitative assessment of new technologies in accordance with BAT principles, development of "Methodology for the quantitative assessment of new technologies for the production of organic substances in accordance with BAT principles."

**P.V. Kazakov** – development of technology for obtaining tetramethylthiuram disulfide, industrial introduction of technologies for obtaining tetramethylthiuram disulfide, *N*-cyclohexyl-2-benzothiazolylsulfenamide, diisopropyl xanthogen disulfide, and *N*-phenyl-2-naphthylamine.

**M.M. Antonova** – development and industrial implementation of technologies for the production of diisopropyl xanthogen disulfide and *N*-phenyl-2-naphthylamine.

**D.I. Klimov** – development and industrial implementation of technologies for the production of *N*-cyclohexyl-2-benzothiazolylsulfenamide and *N*-phenyl-2-naphthylamine.

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#### About the authors:

**Natalya A. Kostikova**, Cand. Sci. (Eng.), Associate Professor, Head of Department, State Research Institute of Organic Chemistry and Technology (GosNIIOKhT), State Scientific Center of the Russian Federation (23, sh. Entuziastov, Moscow, 111024, Russia). E-mail: kutkin@gosniiokht.ru. RSCI SPIN-code 1540-8520, <https://orcid.org/0000-0001-8796-124X>

**Elena N. Glukhan**, Dr. Sci. (Eng.), Assistant Professor, Adviser to the Director-General, State Research Institute of Organic Chemistry and Technology (GosNIIOKhT), State Scientific Center of the Russian Federation (23, sh. Entuziastov, Moscow, 111024, Russia). E-mail: dir@gosniiokht.ru. Scopus Author ID 8706397600, RSCI SPIN-code 6274-1908, <https://orcid.org/0000-0002-2369-5648>

**Pavel V. Kazakov**, Dr. Sci. (Chem.), Assistant Professor, Deputy General Director, State Research Institute of Organic Chemistry and Technology (GosNIIOKhT), State Scientific Center of the Russian Federation (23, sh. Entuziastov, Moscow, 111024, Russia). E-mail: kutkin@gosniiokht.ru. RSCI SPIN-code 1920-2930, <https://orcid.org/0000-0001-8164-274X>

**Mariya M. Antonova**, Cand. Sci. (Eng.), Head of the Research Department, State Research Institute of Organic Chemistry and Technology (GosNIIOKhT), State Scientific Center of the Russian Federation (23, sh. Entuziastov, Moscow, 111024, Russia). E-mail: kutkin@gosniiokht.ru. Scopus Author ID 56165662600, RSCI SPIN-code 4136-5290, <https://orcid.org/0000-0001-6492-2483>

**Dmitry I. Klimov**, Cand. Sci. (Eng.), Head of Sector, State Research Institute of Organic Chemistry and Technology (GosNIIOKhT), State Scientific Center of the Russian Federation (23, sh. Entuziastov, Moscow, 111024, Russia). E-mail: kutkin@gosniiokht.ru. RSCI SPIN-code 7113-2691, <https://orcid.org/0000-0002-0649-1440>

#### Об авторах:

**Костикова Наталья Алексеевна**, к.х.н., начальник отдела, ФГУП «Государственный научно-исследовательский институт органической химии и технологии» (ФГУП «ГосНИИОХТ»), Государственный научный центр Российской Федерации (111024, Россия, Москва, шоссе Энтузиастов, 23). E-mail: kutkin@gosniiokht.ru. SPIN-код РИНЦ 1540-8520, <https://orcid.org/0000-0001-8796-124X>

**Глухан Елена Николаевна**, д.т.н., доцент, советник генерального директора, ФГУП «Государственный научно-исследовательский институт органической химии и технологии» (ФГУП «ГосНИИОХТ»), Государственный научный центр Российской Федерации (111024, Россия, Москва, шоссе Энтузиастов, 23). E-mail: dir@gosniiokht.ru. Scopus Author ID 8706397600, SPIN-код РИНЦ 6274-1908, <https://orcid.org/0000-0002-2369-5648>

**Казаков Павел Васильевич**, д.х.н., доцент, заместитель генерального директора, ФГУП «Государственный научно-исследовательский институт органической химии и технологии» (ФГУП «ГосНИИОХТ»), Государственный научный центр Российской Федерации (111024, Россия, Москва, шоссе Энтузиастов, 23). E-mail: kutkin@gosniokht.ru. SPIN-код РИНЦ 1920-2930, <https://orcid.org/0000-0001-8164-274X>

**Антонова Мария Михайловна**, к.х.н., начальник научно-исследовательского отделения, ФГУП «Государственный научно-исследовательский институт органической химии и технологии» (ФГУП «ГосНИИОХТ»), Государственный научный центр Российской Федерации (111024, Россия, Москва, шоссе Энтузиастов, 23). E-mail: kutkin@gosniokht.ru. Scopus Author ID 56165662600, SPIN-код РИНЦ 4136-5290, <https://orcid.org/0000-0001-6492-2483>

**Климов Дмитрий Игоревич**, к.х.н., начальник сектора, ФГУП «Государственный научно-исследовательский институт органической химии и технологии» (ФГУП «ГосНИИОХТ»), Государственный научный центр Российской Федерации (111024, Россия, Москва, шоссе Энтузиастов, 23). E-mail: kutkin@gosniokht.ru. SPIN-код РИНЦ 7113-2691, <https://orcid.org/0000-0002-0649-1440>

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